

## Structural Calculations for:

# **Chitturi Addition**

3719 82<sup>nd</sup> Ave SE Mercer Island, WA 98040



Job #: 02295-2021-01

Date: October 15, 2021



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Beaux Arts Village

### **Criteria Sheet**

#### Codes

**Project Location** 

Structural IBID@01818

Street & Number 3719 82nd Ave SE

Loading ASCE 7-16

City: Mercer Island State: WA

Wood: NDS 2018

ZIP: 98040

Steel: AISC 360-16 Concrete: ACI 318-14

Latitude: Longitude:

Masonry: TMS 402/602-16

-122.2301 W **Ground Elevation** 

W

258 ft

47,5770 N

#### **Occupancy Category**

Risk Category: II ||

ASCE 7 Table 1.5-1

#### Seismic Load Summary:

Analysis Procedure: Equivalent Lateral Force Procedure

Lateral System: Light-frame (wood) Walls Sheathed with Wood

Structural Panels Rated for Shear Resistance

R: 6.50

C<sub>d</sub>= 4

Base Shear V = 3 klps

Ω<sub>0</sub>= 2.5

S<sub>s</sub>= 1.41 S<sub>ps</sub>= 1.00 S<sub>1</sub>= 0.49

C<sub>s</sub>= 0.154

Spi= 0.59 J<sub>E</sub>= 1.0.

#### Story Information

# Stories Above Grade (including Mezzanine Levels)

Horizontal and Vertical Irregularities:



### Wind Load Summary:

V= 97 K<sub>21</sub>= 1,30

Exposure = B

Is the building a "Regular Structure"? (No horizontal or vertical irregularities)

#### Dead Loads:

.oaus,			
Roof.		Floor	
Roofing	2.5 psf	Finish Floor	1 psf
1/2" Sheathing	1.8 psf	3/4" Sheathing	2.7 psf
Rafters @ 24" oc	2.4 psf	Joists @ 16" oc	2.2 psf
Misc./Mech.	1.5 psf	Misc./Mech.	1.3 psf
Ceiling Finish	2.8 psf	Ceiling Finish	2.8
Solar Panels	4	-	10.0 psf
	15.0 psf	Use	10 psf
Use	15 psf		. •

#### Live Loads:

Snow	25	psi
Floar	40	psi
Deck	60	psi

Soils:

Soils Report Provided?

No

To be approved by the authority having jurisdiction, per 11.8.2 exception.

Allowable Bearing

1500

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### Seismic Design

ASCE 7-16 Seismic Analysis

Equivalent Lateral Force Procedure

	<del></del>		•
Selsmic Force Resisting System Per	System	Bearing Wall Systems	t
Table 12,2-1	System		ĺ
		Light-frame (wood) Walls Sheathed with Wood Structural Panels Rated for Shear Resistance	ĺ
	Type:	Light-raine (wood) wants affecting with wood attraction railess rated for affect resistance	ı
			ı

t. D	Seismic Design Cat.
y II	Risk Category
s D (Default)	Site Class
y Frexible	Diaphragm Flexibility

l, II, or III, or IV per Table 1.5-1 Assumed default soil properties, per 11.4.3.

		4	
·S <sub>s</sub>	1.41 g		de & Longitude lookup
S <sub>1</sub>	0.49 g	2% in 50 yr, Latitu	de & Longitude lookup
R	6.50		
C,	4.0		
$\Omega_{o}$	2.5		
l <sub>e</sub>	1.00	Table 1.5-2	
h <sub>n</sub>	18.5 ft	1	
Ct	0.02	Table 12,8-2	
X	0.75	Table 12.8-2	Building Period Per
T <sub>a</sub>	0.18 sec		Alternate Analysis
T	0.18 sec	Eq. 12.8-7	T (sec)
To	0.12 sec		
Ts	0.59 sec	1	
TL	6.00 sec		Per Geotech Report
F.	1.20	Table 11.4-1	F <sub>a</sub>
F <sub>v</sub>	1.81	Table 11.4-2	F <sub>v</sub>
S <sub>MS</sub>	1.69 g	Eq. 11.4-1	<u> </u>
S <sub>Mt</sub>	0.89 g	Eq. 11:4-2	
Sps	1.000 g	Eq. 11.4-3	
S <sub>D1</sub>	0.591 g	Eq. 11,4-4	
		1	
AMERICAN PROPERTY OF THE PARTY	0.154 Controls	Eq. 12.8-2	
C,	0.510	Eq. 12.8-3 need no	ot exceed, T < T
-	0.010	Eq. 12.8-5 or 12.8-	6 minimum
C <sub>s</sub> , design	0.154	Section 11.4.8 Exc	eption 2 Applied

#### Section 12.8.1.3 Exceptions

Regular Structure	Yes
≤ 5 Stories above grade	Yes
T ≤ 0,5s	Yes
p = 1.0	Yes
Not Site Class E or F	Yes
Risk Category I or II	Yes

If all exceptions are met,  $S_{DS}$  may be taken as 1, but not less than 0.7 (Calculated  $S_{DS}$ )

$T_a = C_t h_n^x$	Eq. 12.8.7
$S_{MS} = F_{\alpha}S_{S}$ $S_{M1} = F_{\nu}S_{1}$ $S_{DS} = \frac{2}{3}S_{MS}$ $S_{D1} = \frac{2}{3}S_{M1}$	Eq. 11.4-1 Eq. 11.4-2 Eq. 11.4-3 Eq. 11.4-4
$C_{S} = \frac{S_{DS}}{(R/I_{e})}$ $C_{S} = \frac{S_{D1}}{T(R/I_{e})}$ $C_{S} = \frac{S_{D1}T_{L}}{T^{2}(R/I_{e})}$ $C_{S} \ge 0.044S_{DS}I_{e}$ $C_{S} \ge 0.01$	Eq. 12.8-2 Eq. 12.8-3 Eq. 12.8-4 Eq. 12.8-5 Eq. 12.8-5

$C_{VX} = w_x h_x^k / \sum_{i=1}^n w_x h_i^k$	Eq. 12.8-12
$F_{px} = \frac{\sum_{i=x}^{n} F_i}{\sum_{i=x}^{n} w_i} w_{px}$	Eq. 12.10-1
$F_{px} \ge 0.2 S_{DS} I_e w_{px}$	Eq. 12.10-2
$F_{px} \le 0.4 S_{DS} I_e w_{px}$	Eq. 12.10-3

Vertical Distrib	ution	ASSID	ρ≕	11	k≍	1.000						
Level	h <sub>x</sub> (ft)	W <sub>x</sub> (k)	h <sub>x</sub> <sup>k</sup> (ft)	W <sub>x</sub> h <sub>x</sub> <sup>k</sup>		Story Shea ASD	r		Forc	Diaphragm e (p not incl	uded)	
					C <sub>vx</sub> (%)	F <sub>x</sub> (k)	SV (k)	F <sub>px,calc</sub>	F <sub>px,mln</sub>	F <sub>рх,тах</sub>	F <sub>px.design</sub>	γ=F <sub>px</sub> /F <sub>x</sub>
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				***************************************	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	***************************************	- 11. tanii - adalaan dadda kanan kan					VMF. 555557711 5 7074
Roof Add	18.5	7.64	18.5	141	0.637	1.1	1.1	1.1	1.1	2.1	1.1	1.00
2nd Add	9.0	9	9.0	81	0,363	0.6	1.8	1.0	1.3	2.5	1.3	1.93
Σ		16.6		222		1.8						

Eq. 12.8-1, Strength Level Base Shear

Eq. 12.8-1 ASD Base Shear



Bldg. Weight

 $V = C_s W$ 

 $V = C_{Sasd}W$ 

16.6 k

2.6 k

1.8 k

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# Wind Design - MWFRS ASCE 7 Chapter 27 - Directional Procedure

Design Method	ASDASD

### Wind Coefficients

Exposure	Вв	
V=	97	mph
K <sub>e</sub> =	0.85	Table 26.6-1
K <sub>n</sub> =	0.61	Table 26.10-1
K <sub>e</sub> =	0.99	Table 26.9-1
G=	0.85	26.9.4

### Transverse Wind Pressures

L/B = 0.68

h/L = 0.36

Pressure Coefficients from Figure 27.3-1:

Bldg Face	C <sub>p</sub>
Windward Wali	0.8
Leeward Wall	-0.50
Windward Roof	-0.44 / 0.03
Leeward Roof	-0.56

#### Location and Building Dimensions

0.1.1.1.17.101		1
Calculate Kzt?	NdNo	
Kzt	1.30	
Roof Type	Hilbip.	
Roof Angle - Transverse Dir	18	degrees
Roof Angle - Long Dir	18	degrees
Ground to top of roof	21	ft
Bot of roof to top of roof	5	ft
Mean Roof Height, h	18.5	ft
Short Plan Dimension	51	ft.
Long Plan Dimension	75.5	ft
Parapet?	Ифіо	
Control of the Contro	ayan da ayan d	

<del></del>		
Velocity Pressure at Mean	16.1	psf
Roof Height, q <sub>n</sub> =	10.1	21

### Wall Pressures (Unfactored);

ASĐ

	Roof Press	ures (Unfact	ored)	ASD
1	Winc	dward	Laguered	Horiz Proj
1	Max	Min	Leeward	(psf)
ł	0,5	-6,1	-7.7	4,80

Ht	K <sub>z.</sub>	q,	Pww.weits	Piwwalls	P <sub>walls</sub> (pst)
0-15	0.57	15.03	10.22	6.84	10.2
15-20	0,62	16,35	11,12	6.84	10.8
20-25	0.66	17.40	11.83	6.84	11.2
25-30	0.7	18.46	12.55	6.84	11.6
30-40	0.76	20.04	13.63	6:84	12.3
41-50	0.81	21.36	14.52	6.84	12.8
51-60	0.85	22.41	15.24	6.84	13.2
61-70	0.89	23.47	15.96	6.84	13.7
71-80	0.93	24.52	16.68	6.84	14.1
81-90	0.96	25.31	17.21	6.84	14.4
91-100	0.99	26.11	17.75	6.84	14.8

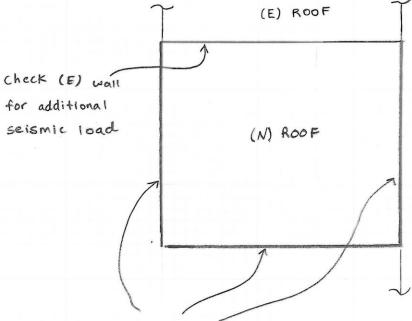
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Chitturi Addition	
Wind Criteria	

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# LATERAL SCOPE

AT ROOF LEVEL .



(E) BREEZEWAY

(E) GARAGE

Design (N) walls for addition seismic wind loads

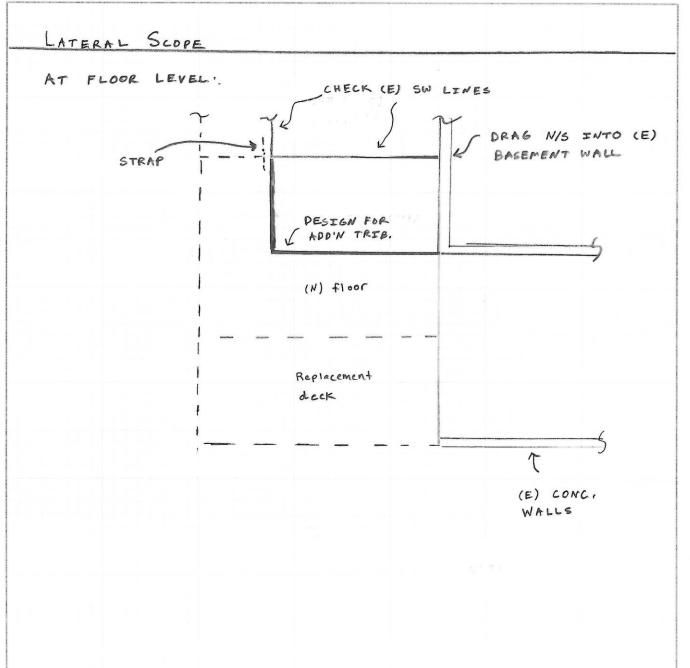
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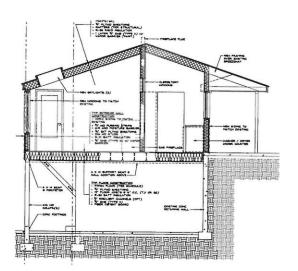
DESIGN L1

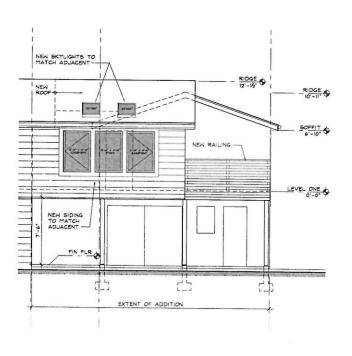


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DESIGN L2





No change in wind area

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Open below, only change in wind surface area is at 2nd fibor and minimal

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DESIGN L3

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# LATERAL DESIGN

## SEISMIL WEIGHT

DL ROOF = 15 psf

DL FLOOR/DECK = 10 psf

DL PARTITIONS = 5 psf @ roof level 10 psf @ floor level

ADDITION (i.e. new construction) SEISMIC WT:

WROOF = 382 \$ x (15 psf roof + 5 psf part.) = 7640 #

Wand = 350 \$ x (10 psf floor + 10 psf part.) +196 \$ x 10 psf deck = 8960 #

SEE PAGE 2 FOR SEISMIC PARAMETERS AND VERT. DIST

VADDIN = 1.8 K ASD

## WIND PRESSURES

SIMPLIFY W/ TRANSVERSE (WORST CASE) WALL WIND PRESSURES WN/S, ROOF = 4.5' wall average = 10.8 psf = 49 pif ASD WN/s, FLOOR = (4.5' wall average + 1' diaph.) x 10.2 psf = 56 plf ASD

WEIN, ROOF = 3.5' WALL x 10.8 psf + 5 'x 4.8 psf roof = 62 pif ASD WE/W, FLOOR = (3.5' Wall + 1' diaph.) x10. 2 PSF = 46 pif ASD



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L4

## ROOF SHEARWALLS

SEE PG. LI FOR IMAGE OF WALLS BEING CHECKED

N/S SHEARWALLS:

	1100#/251 = 44 p1f			
	W	20.	0 5,	E
LOAD	440		660	
LENGTH	6.5'		5.75'	
SHEAR	68	115		
WALL	W6	W6		
0 T	475	800		
H D	C516	CSIB		

E/W SHEARWALLS:

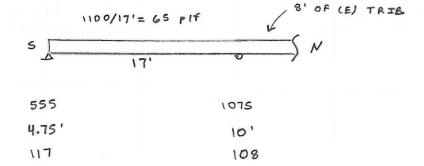
LOAD

LENGTH

SHEAR

WALL

H-D



500

WB

850

0516

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(E) GYP. VALL = 145 PIF

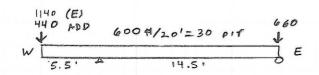
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## FLOOR SHEARWALLS

SEE PG. LZ FOR IMAGE OF WALLS BEING CHECKED

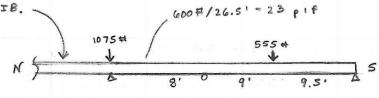
N/S SHEARWALLS:



LOYD	2600	250
LENGTH	23.5	16'
SHEAR	111	16
WALL	(E) gyp.	(E) CONC.
OT	-	-
HD	-	-

8' OF (E) TRIB. .

E/W SHEARWALLS:



LOAD	1090	965	370
LENGT H	8.75	14'	23'
SHEAR	125	69	16
WALL	(E) 94P.	W6	(E) CONC.
OT	_	550	-
HD	-	HDU2	_



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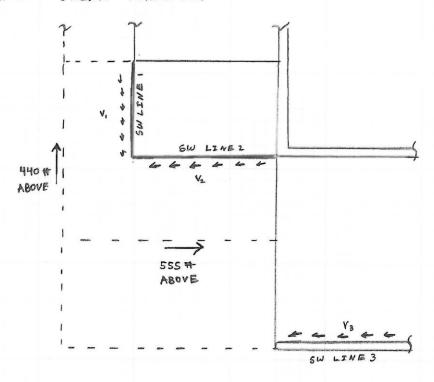
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VALL = 180 x 0,93 HF = 167 pif ASD

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ROJ. # TCV

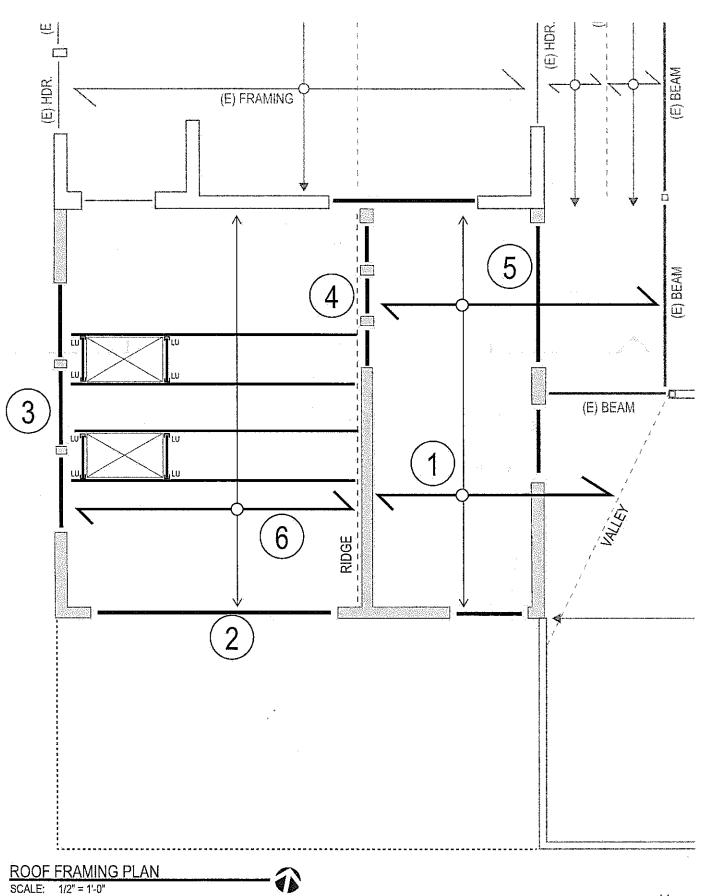
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# **Roof Framing Key Plan**



# VERTICAL FRAMING

# ROOF FRAMING

1 2×12 @ 24" 00

 $W = 2' \times 40 \text{ psf} = 80 \text{ pif}$  M = 1103 #-FT R = 138 #  $R_2 = 862 \text{ #}$   $f_b = 418 \text{ psi}$   $f_v = 39 \text{ psi}$   $\Delta = 0.11'', L/1131$ 

(2) 2×8 HF #2

L=10.5'

W= 2'x 40 psf = 80 psf

M= 1103 #-FT

R= 420 #

fb= 503 psi

fv= 30 psi

\$\Delta = 0.18'' \frac{1}{13}

D = 15 psf S= 25 psf TL= 40 psf

(2) 2×8 HF #2

L=3.25'

W=7'×40psf=280pif

M= 370 #-FT

R= 455 #

fb= 169 psi

fv= 31 psi

A= 0.01"

(2) 2×8 HF #2

L= 2'

W=10×40 psf = 400 p1f

M= 200 #-FT

R= 400 #

fb= 91 psi

fv= 28 psi

A = 0"



CHITTURE ADDITION

PROJ. #

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# ROOF FRAMING (CONT.)

- (2) 2 × 8 HF # 2 L=6' W=6.5' × 40 psf = 260 pif M=1170 #-FT R= 780 # fb= 534 psi fv= 54 psi A = 0.06", L/1176
- © 2×12@ 24" 0 €

  L = 13'

  W = 2'×40 psf = 80 psf

  M = 1640 #-FT

  R = 520 #

  fb = 641 psi

  fv = 46 psi

  Δ = 0.15", L/10 so

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CHITTURE ADDITION

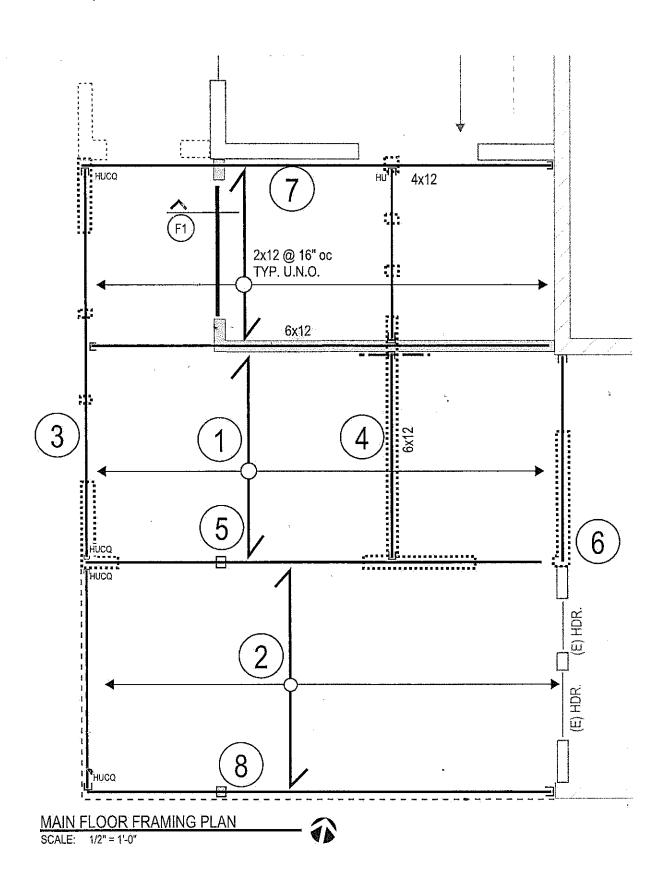
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SHEE

# **2nd Floor Framing Key Plan**



# VERTICAL FRAMING

## 2ND FLOOR FRAMING

D=10 psf L=40 psf LDECK = 60 psf

1 2×12 HF #2 @ 16" oc

L = 9'

W= 50 psf x 1.331 = 67 plf

M = 678 #-FT

R= 302 \$

fb = 257 psi

fv = 27 psi

A = 0.04", 4/2526

2 2x10 HF #2 @ 16"

L= 10'

W = 70 psf x1.33' = 93 pif

M= 1163 #-FT

R = 465 #

fb = 652 psi

fr = 50 psi

A = 0.16", 4/738

3 6×12 DF #1

1 1030 4

W= 6.5' x 40 esf = 260 pif

M= 13.0 K-FT

R = 2613 +

R2= 2707 H

fb= 1285 ps:

fr= 64 psi

A= 0.43", 4/461

4) 4×12 DF #1

1=91

W = 10' roof x 40 psf + 12' Wall x 10 psf -

= 520 pif

M= 5265 #-FT

R= 2340#

fb = 856 psi

fv= 89 psi

A = 0.11", 4993



CHITTURE ADDITION

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# 2ND FLOOR FRAMING (CONT.)

5 PSL 5/4 x 11/4

w= 5'x70 psf + 4.5'x 50 psf = 575 pff

M= 23.1 K-FT

R,= 3.5 K

R2- 12.6 K -

fb= 2499 psi

fr= 173 psi

A= 0.39",4/336

3'-0" SQ. FTG.

RALL= 9 FT2 x 1500 psf

= 13500 #

6 6x10 DF #1

W= 8.5' wall x 12 psf + 8624 rafter = 533 ptf

M= 6.3 K-FT

R= 5.7K

P2 = 2.6 K

fb= 915 psi

fr = 164 psi

A = 0.15" L/722

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# 2ND FLOOR FRAMING (CONT.)

## (1) 6×12 DF #1

W= 4' + 50 pst = 200 prf

M= 14.1 k-FT

R1 = 5.5 K

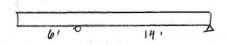
R2 = 0.4 K

fb = 1465 psi

fv = 76 psi

A = 0.49", 4/267

# 8 6x10 DF #1



W= 5'x70 psf = 350 psf
M= 6300 #-FT

R= 5000 #

R2= 2000 #

fb= 914 psi
fv= 83 psi
A= 0.21", -/617

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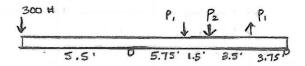
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#### (3) TRANSFER BEAM - LATERAL

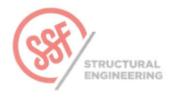
CHECK PSL 5 1/4 x 11/4 @ 2ND FLOOR FOR HD FORCE W/ N= 2.5

1.140 + 2.5 x (0.7 x E)

PSL 51/4 x 11/4



W= 1.14 x 5' x 10 psf = 57 pif P, = 2.5 x 850 # E = 2125 # E P2= 1665 DL M = 8900 #-FT R,= 2765 # R2= 340 # fb= 965 psi fr = 57 psi A= 0.19", 4/906



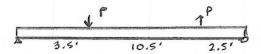
CHITTURE RESIDENCE

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TCV V8

# TRANSFER BEAMS - LATERAL 3

PSL 5/4 x 11/4



 $P = 2.5 \times 47S = 1190 \# ASD (D=2.5)$   $W = 6.5' \times 15 psf roof \times 1.14 = 111 prf$  M = 5216 # FT  $R_1 = 1673 \#$   $R_2 = 158 \#$   $f_b = 565 psi$   $f_v = 42 psi$   $\Delta = 0.18", 4/1127$ 

1/21

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